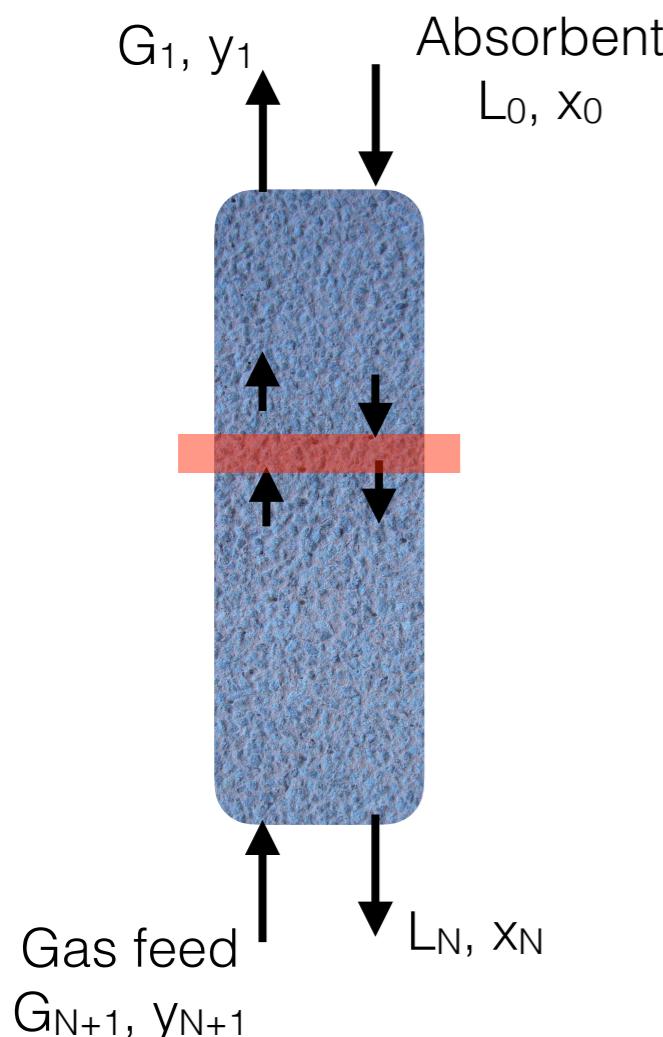


# Review quiz

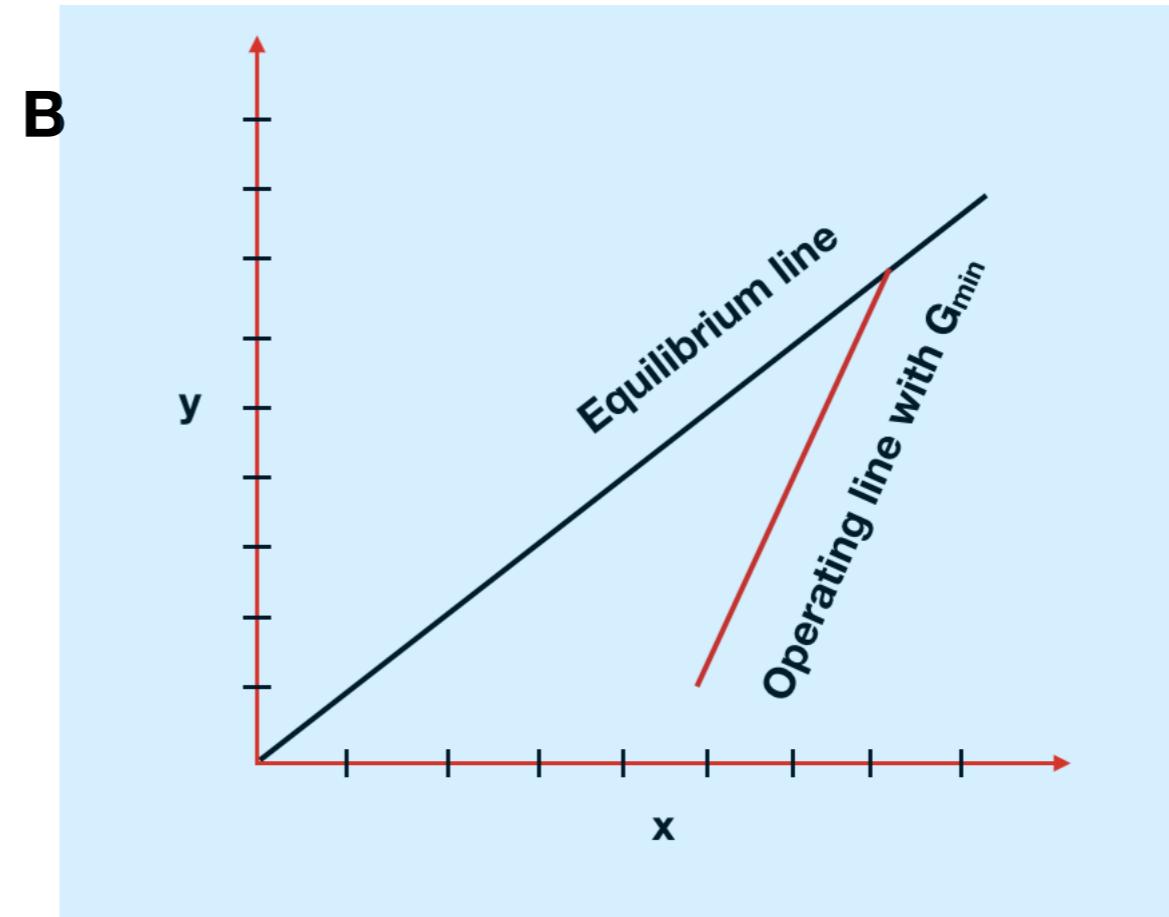
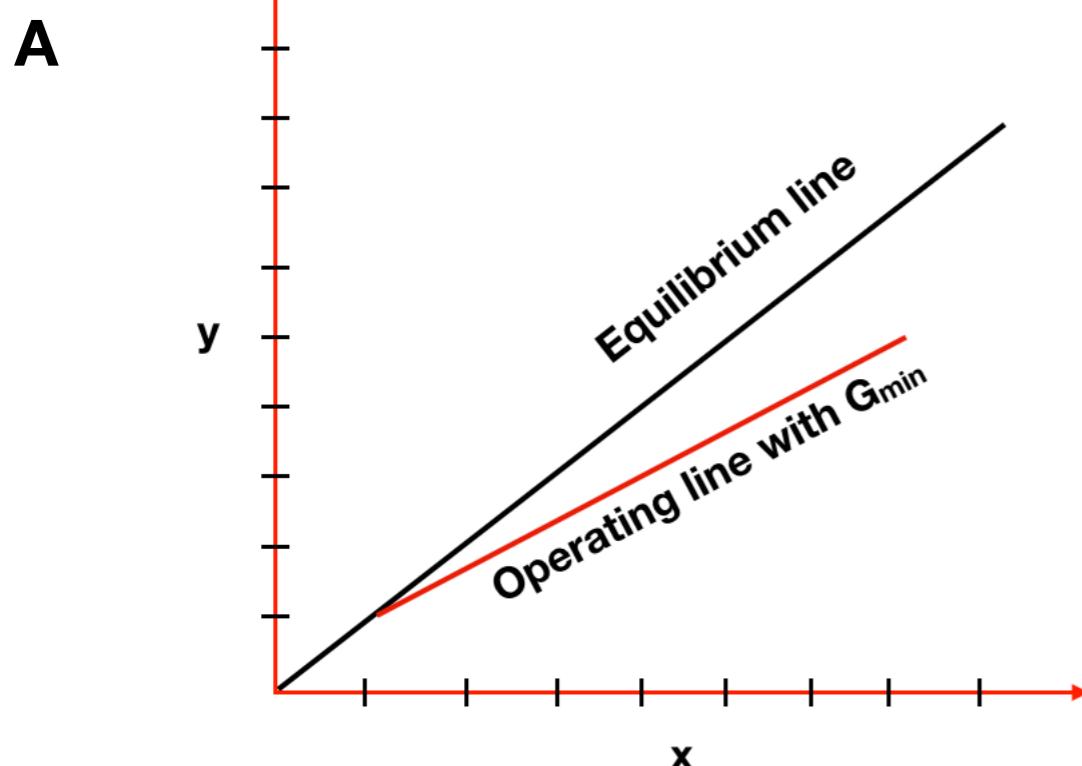
Consider the following case of mass balance on an absorption column where a gas is being absorbed. Which of the following statements is incorrect.



- A.  $G_1 > G_{N+1}$
- B.  $G_1 < G_{N+1}$
- C.  $L_0 < L_N$
- D. Mass transfer takes place from gas to liquid

# Review quiz

Which one of the following represents minimum gas flow rate for stripping (countercurrent operation)

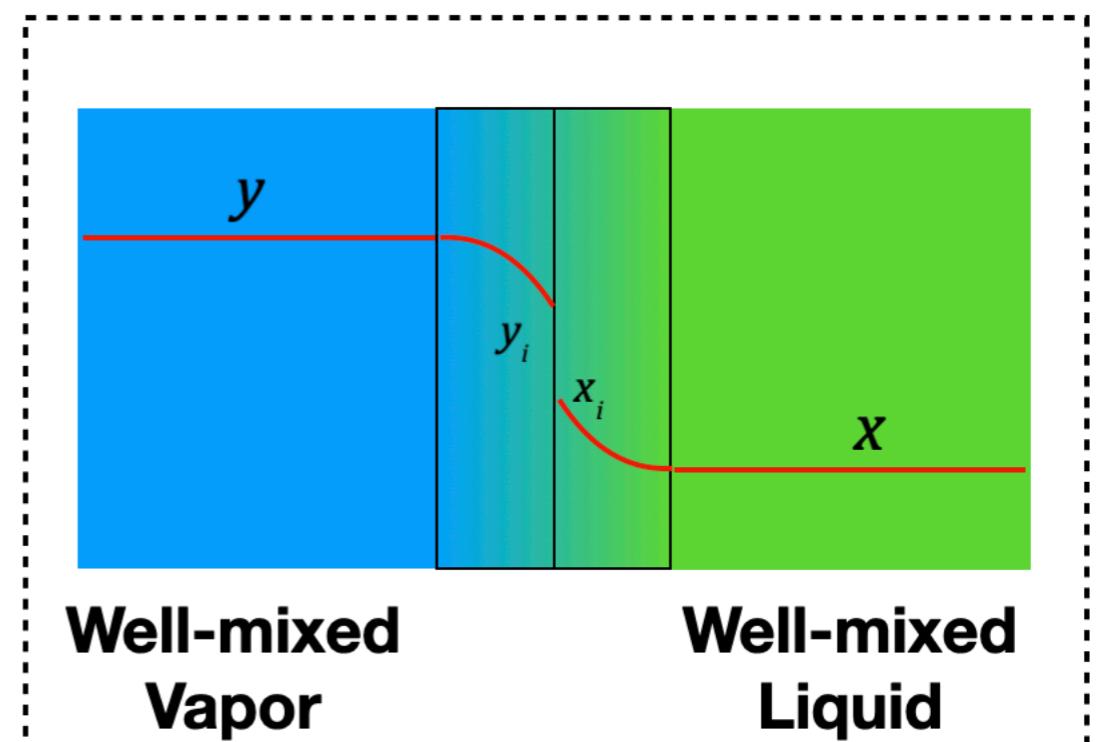


# Review quiz

In the following expression, which one of the statements is not true

$$N = K_y A (y - mx) = K_x A \left( \frac{y}{m} - x \right)$$

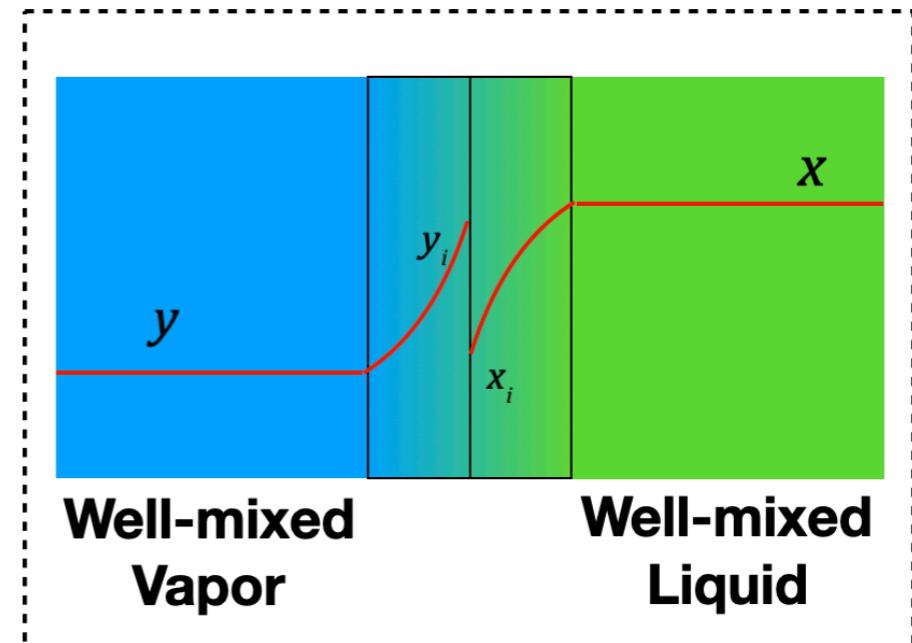
- A.  $y = y_i$
- B.  $x = x_i$
- C.  $x$  and  $y$  are not interfacial concentrations
- D.  $K_x = K_y$



# Review quiz

What is the direction of mass transfer in this case?

- A. Vapor to liquid.
- B. Liquid to vapor.
- C. Both directions.
- D. The net mass transfer is zero.



# In-class exercise problem

A natural gas from a well in offshore Norway has CO<sub>2</sub> concentration of 3% (molar basis). CO<sub>2</sub> needs to be captured and sequestered to curb global warming. Therefore, the gas needs to be treated to reduce CO<sub>2</sub> concentration to 0.1%. For this, you decided to create a pilot plant test using a packed bed absorption column contacting with liquid amine at 25 °C in a countercurrent fashion. The height of column is 1.0 meter and its cross-sectional area is 0.1 m<sup>2</sup>. An amine is available as an absorbent but has 0.01% of CO<sub>2</sub>. The equilibrium relationship for absorption of CO<sub>2</sub> in the amine can be described by  $y_i = mx_i$  where  $m = 2$ . You decided to use 100 mole/s of this amine absorbent to treat 10 mole/s of natural gas. You have designed the system to perfection and equilibrium is established at the contact between the gas phase and the liquid phase. Assuming the case of dilute absorption:

1. Calculate the concentration of CO<sub>2</sub> in the outlet stream of the amine.
2. Calculate HTU and NTU.
3. Calculate the gas phase overall mass transfer coefficient, K<sub>ya</sub>.

$$L(x_N - x_0) = G(y_{N+1} - y_1)$$

$$y_{N+1} = 0.03$$

$$y_1 = 0.001$$

$$x_0 = 0.0001$$

$$x_N = x_0 + \frac{G}{L}(y_{N+1} - y_1)$$

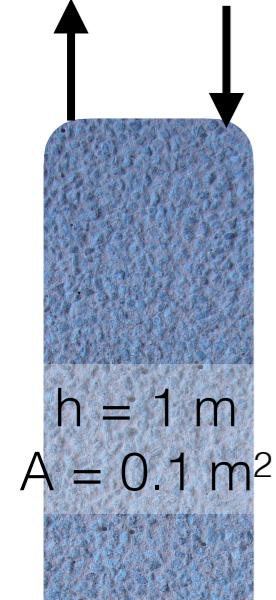
$$G = 10 \text{ mole/s}$$

$$L = 100 \text{ mole/s}$$

$$\Rightarrow x_N = 0.0001 + 0.1 * 0.029 = 0.003$$

$$y_1 = 0.001 \quad x_0 = 0.0001$$

$$NTU = \left( \frac{1}{1 - \frac{mG}{L}} \right) \ln \left( \frac{y_{N+1} - mx_N}{y_1 - mx_0} \right) = \left( \frac{1}{1 - \frac{2*10}{100}} \right) \ln \left( \frac{0.03 - 2 * 0.003}{0.001 - 2 * 0.0001} \right) = 4.25$$



$$h = HTU * NTU$$

$$\Rightarrow HTU = h/NTU = 1/4.25 = 0.23 \text{ m}$$

$$HTU = \frac{G}{K_y a A} = \frac{10}{K_y a * 0.1}$$

$$\Rightarrow K_y a = 100/HTU = 425 \text{ mol/m}^3\text{/s}$$

# In-class exercise problem

Consider the problem of countercurrent absorption of a gas (dilute in concentration) in a liquid absorbent. Derive an expression for the needed height of the column in terms of the adsorbent flow rate (L) and the overall mass transfer coefficient on the liquid side ( $K_x$ ).

Hint: setup mass transfer as we did in the lecture video. The final expression should be

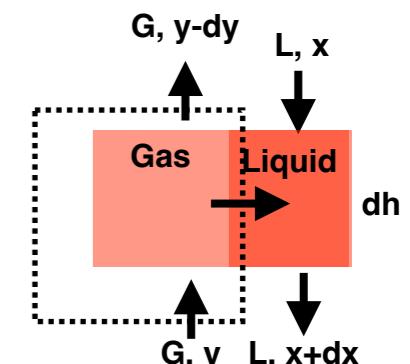
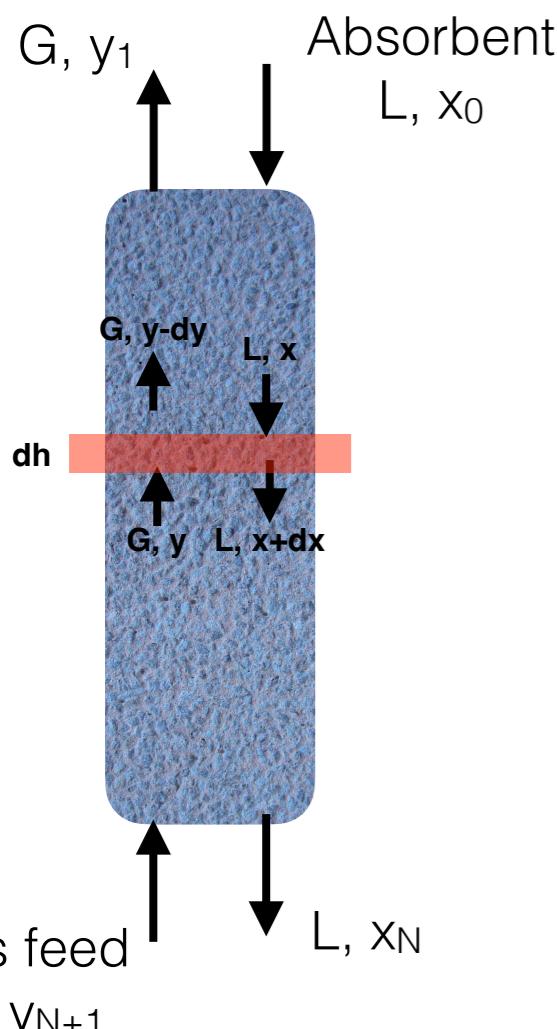
$$h = \frac{L}{K_x a A} \left[ \left( \frac{1}{\frac{L}{mG} - 1} \right) \ln \left( \frac{y_{N+1} - mx_N}{y_1 - mx_0} \right) \right]$$

## Overall balance on the element

Accumulation = in - out

$$0 = (Gy + Lx) - (G(y-dy) + L(x+dx))$$

$$Gdy = Ldx$$



## Applying mass transfer concept

Accumulation = in - out

$$x^* = y/m$$

$$0 = Lx + K_x(x^* - x)aAdh - (x + dx)L$$

$a$  = surface area per unit volume

$Adh$  = volume available for mass exchange

$$\Rightarrow \int_{x_0}^{x_N} \frac{L}{K_x a A} \frac{dx}{\left( \frac{y}{m} - x \right)} = \int_0^h dh$$

$$\Rightarrow h = \int_{x_0}^{x_N} \frac{L}{K_x a A} \frac{dx}{\left( \frac{y}{m} - x \right)}$$

**EPFL**

$$\Rightarrow h = \int_{x_0}^{x_N} \frac{L}{K_x a A} \frac{dx}{\left( \frac{y}{m} - x \right)}$$

substitute  $y = \frac{L}{G}x + \left( y_1 - \frac{L}{G}x_0 \right)$

$$\Rightarrow h = \frac{L}{K_x a A} \int_{x_0}^{x_N} \frac{dx}{\left( \frac{1}{m} \left[ \frac{L}{G}x + \left( y_1 - \frac{L}{G}x_0 \right) \right] - x \right)}$$

$$\Rightarrow h = \frac{L}{K_x a A} \int_{x_0}^{x_N} \frac{dx}{\left[ x \left( \frac{L}{mG} - 1 \right) + \left( \frac{y_1}{m} - \frac{L}{mG}x_0 \right) \right]}$$

$$\Rightarrow h = \frac{L}{K_x a A} \frac{1}{\left( \frac{L}{mG} - 1 \right)} \ln \left[ \left( \frac{L}{mG} - 1 \right) x + \frac{y_1}{m} - \frac{L}{mG} x_0 \right] \Big|_{x_0}^{x_N}$$

$$\Rightarrow h = \frac{L}{K_x a A} \frac{1}{\left( \frac{L}{mG} - 1 \right)} \ln \left[ \frac{\left( \frac{L}{mG} - 1 \right) x_N + \frac{y_1}{m} - \frac{L}{mG} x_0}{\left( \frac{L}{mG} - 1 \right) x_0 + \frac{y_1}{m} - \frac{L}{mG} x_0} \right]$$

$$\int (ax + b)^{-1} dx = \frac{\ln(ax + b)}{a}$$

$$\Rightarrow h = \frac{L}{K_x a A} \frac{1}{\left( \frac{L}{mG} - 1 \right)} \ln \left[ \frac{\cancel{\left( \frac{L}{mG} - 1 \right)} x_N + \frac{y_{N+1}}{m} - \cancel{\frac{L}{mG} x_N}}{\cancel{\left( \frac{L}{mG} - 1 \right)} x_0 + \frac{y_1}{m} - \cancel{\frac{L}{mG} x_0}} \right]$$

$$h = \frac{L}{K_x a A} \left[ \left( \frac{1}{\frac{L}{mG} - 1} \right) \ln \left( \frac{y_{N+1} - mx_N}{y_1 - mx_0} \right) \right]$$

From operating line

$$y_1 - \frac{L}{G}x_0 = y_{N+1} - \frac{L}{G}x_N$$